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Verification of Monitor Unit Calculations for Eclipse Treatment Planning System by in-House Developed Spreadsheet

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| ARTICLE INFO | ABSTRACT |
|--|---|
| Article type: Original Article | <i>Introduction</i> : Computerized treatment planning is a rapidly evolving modality that depends on hardware and software efficiency. Despite ICRU recommendations suggesting 5% deviation in dose |
| <i>Article history:</i> Received: Apr 05, 2017 Accepted: Nov 10, 2017 | delivery the overall uncertainty shall be less than 3.5% as suggested by B.J. Minjinheer. J. In house spreadsheets are developed by the medical physicists to cross-verify the dose calculated by the Treatment Planning System (TPS). <i>Materials and Methods:</i> The monitor unit verification calculation (MUVC) verification was tested for |
| Keywords: Radiotherapy Planning Computer Assisted Radiotherapy Padiotherapy Dosage | pre-approved and executed treatment plans taken from the TPS. A total of 108 square fields and 120 multileaf-collimators (MLC) shaped fields for Head & Neck cancers, cervical and esophageal cancers were taken for evaluation. In house developed spreadsheet based on Microsoft Excel was developed. The dose calculation parameters such as Output Factor (O.F), Percentage Depth Dose (PDD) and off axis ratio (OAR) data were taken from the TPS. |
| Radiotierapy Dosage | Results: The overall MU ratio fell within the range of 0.999 to 1.02 for square field geometries showing deviation of 1% between the TPS calculation and the spread sheet calculation. The MU ratios were 0.995 for Head & Neck plans & 1.012 for cervix plans with the standard deviation of 0.024 & 0.029 respectively. However we observed the mean MU ratio for Esophagus plan was 1.026 with the standard deviation of 0.040. |
| | <i>Conclusion:</i> The spreadsheet was tested for most of the routine treatment sites and geometries. It has good agreement with the Eclipse TPS version 13.8 for homogenous treatment sites such as head & and neck and carcinoma cervix. |

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Introduction

Radiotherapy is a form of treatment in which ionizing radiations are directed towards the tumor that eradicating the cancer cells. At least 50% of the patients with malignancies require radiotherapy treatment in their course of treatment either exclusively or combined with other modalities [1]. Curative radiotherapy is aimed at providing best local control and preserves the function of normal surrounding structures. The accuracy of the delivered dose must be less than $\pm 5\%$ of the prescribed dose [2, 3, 4].Treatment delivery is associated with daily patient setup, dose calculation & dose delivery. All these parameters are monitored and kept in tight tolerance to achieve overall accuracy. Calculating dose per monitor unit at the calculation point is essential to ensure accurate dose delivery.

In-hand monitor unit calculations can be performed for simple geometry fields. Computerbased calculation is required for advanced techniques such as 3D conformal radiotherapy, and intensity modulated radiotherapy etc. This is accomplished by delivering the suitable radiation dose accurately to the tumor with meticulous computerized planning in the Treatment Planning system (TPS).Computerized treatment planning is a rapidly evolving modality that depends on hardware and software efficiency [5]. Despite various ICRU recommendations suggest 5% deviation in dose delivery the overall uncertainty shall be less than 3.5% as suggested by Minjnheer.[6-8].

TPS is commercially available are available which functions with different techniques to determine dose [9-11]. To ensure accurate dose delivery to the patients independent or secondary verification of monitor units (MU) check is preferred [11-14]. The TPS calculation being a part of overall uncertainty, measures should be taken to reduce the errors in calculation. TPS dose calculation is validated either by hand calculations or by homegrown software [15-17]. Although modern TPS performs sophisticated

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calculations improper use and software faults can result in radiation accidents [18].In house spreadsheets are developed by the clinical medical physicists to cross verify the dose calculated by the TPS. The Task Group 40 &and 114 recommends that the calculation results of any TPS should be independently verified [19-20].The presence and aid of computers will surely reduce the time consumed for manual checks.

The aim of this present work was to develop a spreadsheet program (MS-Excel based) for MU verification calculations (MUVC) for square fields, rectangular fields, as well as complex and irregular shaped photon beams used in 3D conformal radiotherapy. The quantities necessary for dose calculation such as total scatter factor (Sc,p), tissue maximum ratio (TMR)are taken from the measured beam data. We aimed to estimate the accuracy of inhouse developed spread-sheet for MU calculations performed for the conventional and 3D conformal radiotherapy techniques compared with eclipse TPS.

Materials and Methods

The MUVC was tested for pre-approved and executed treatment plans taken from our TPS database (Make: Varian Medical System, Model, Eclipse version 13.7). The treatment plans were made for Linear Accelerator (Make: Varian Medical Systems, Clinac 2100CD, Palo Alto, CA) with [integrated 80 leaf Multileaf collimator] for 6MV Xray beams. The commissioned beam data are present in the TPS for dose calculation. The performance of the TPS was ensured at the time of commissioning by TPS QA test recommended by TRS 430.

In- house developed spreadsheet based on MS-Excel was used in this study. The necessary dose calculation parameters such as Output Factor (O.F), Percentage depth Dose (PDD) and off axis ratio (OAR) data were taken from the TPS. The OF & PDD values were taken for the field sizes of 4x4, 6x6,8x8,10x10,12x12,15x15,20x20,25x25,30x30,35x 35, and 40x40 cm² square field sizes. The OAR values were taken for the same mentioned field sizes at the depths of d_{max} , 5cm, 10cm, 15cm, 20cm and 30cm. These parameters were fed in MS- Excel software and calculation spreadsheet was generated by developing a look- up table.

Calculation Formalism

The calculation formula for MU checks were programmed in the MS-Excel software. A look-up table was framed for PDD values against all the field sizes. The output factors for square fields were fed in the spreadsheet and missing values were obtained through Lagrange interpolation. The parameters mentioned in table 1 were used for calculating MUs.

Calculation Method

SSD Technique

Monitor unit calculations require PDD data as a prime input for determining the MU for SSD beam delivery. The MU required to deliver dose (D) at depth (d) for the field size (A_s) is determined as below in Figure 1.

$$MU = \frac{D \times 100}{D0 \times ScovPDD(dASSD) \times WF \times 0AR}$$
(1)



Figure 1. Dosimetric setup for SSD-based calculation

| Table1 | L.Essentia | l input parameters | required f | or in- | house c | lose ca | lculation |
|--------|------------|--------------------|------------|--------|---------|---------|-----------|
|--------|------------|--------------------|------------|--------|---------|---------|-----------|

| Sr. No | Symbol | of | input | Nomenclature | Definition |
|--------|-----------|----|-------|----------------------------|---|
| 1 | parameter | | | Deres in the second second | |
| T | D | | | Prescribed tumor dose | Dose prescribed per fraction for tumor eradication |
| 2 | D_0 | | | Reference dose rate | Dose rate per MU under normal reference conditions |
| 3 | S_{cp} | | | Total scatter factor | Ratio of dose per MU in phantom for a given field size to that of reference field size |
| 4 | A_d | | | Field size | Field size defined at the depth d |
| 5 | As | | | Field size | Field size defined at the surface |
| 6 | PDD | | | Percentage-depth- dose | ratio of dose rate at depth d, to that of dose rate at d_{max} in water phantom for a given field size defined at source to surface distance |
| 7 | TMR | | | Tissue Maximum Ratio | ratio of dose rate at depth d, to that of dose rate at d_{max} in water phantom for field size defined at SAD |
| 8 | WF | | | Wedge Factor | Wedge factor is the ratio of dose rate at the point of calculation for a wedged field to that for a same field without wedge modifier |
| 9 | OAR | | | Off Axis Ratio | The ratio of the open field dose rate at an off-axis point to that for the same field shifted such that the point of calculation lies on the central axis |



Source to axis distance isocentric technique: The SAD calculations require TMR as the input data and MU calculation is performed as shown in Figure 2.

$$MU = \frac{1}{D0 \times Scp \times TMR(d,Ad_s) \times WF \times OAR}$$
(2)

Isocentric 3D CRT Plans

Verification was performed for sites namely brain, head & neck, esophagus, abdomen, pelvis, prostate and rectum as shown in table 2 . The treatment plans were mainly isocentre based performed by 6MV X-rays. Additionally the MUVC checks are performed for open beam square, rectangular fields along central axis and off axis points for both SSD and SAD techniques.

The majority of the plans were planned on isocentre based; the calculation formula for isocentric method was used for calculating MU for the conformal radiotherapy plans as well. The inputs required for MUVC were effective area (cm²), water equivalent depth (cm), total dose (cGy), and dose per field (cGy), and beam weightings (%) were taken from the TPS. Various planning tools available in the eclipse TPS were used for obtaining the inputs for MUVC verification. The effective area was calculated by creating a field aperture contour in plan parameters workspace (Figure 3).

The obtained effective area was square rooted and side of Equivalent Square was obtained. The water equivalent depth (d_{eff}) is calculated from the Water Equivalent Depth (WED) tool in the TPS (Figure 4); $d_{eff} = d \ge \rho$ is the radiological depth that accounts the mass density (ρ) and distance (d) of the calculation point.



Figure 2. Dosimetric setup for SAD isocentre based calculation



Figure 3. Measurement of effective area from the plan parameter workspace

| | Tab | le 2. Treatment sites taken for monitor unit | verification calculation | |
|-----|---------------|--|--------------------------|--------------------|
| Sr. | Site | Treatment technique | Setup(SAD/SSD) | No of fields taken |
| No | | - | | for MUVC |
| 1 | Head and neck | MLC - based 3D Conformal Technique | SAD | 40 |
| 2 | Esophagus | MLC- based 3D Conformal Technique | SAD | 40 |
| 3 | Cervix | MLC- based 3D Conformal Technique | SAD | 40 |



Figure 4. Calculation of water equivalent depth



Figure 5. Bilateral and lower anterior neck field placement for Head and Neck



Figure 6. Treatment plan for esophageal cancer



Figure 7. Treatment plan for cervical cancer

The effective area and WED were given as input in the spreadsheet; VLOOKUP and HLOOKUP operations from the excel spreadsheet gave values for PDD and TMR. The O.F values were obtained for the square rooted side of equivalent square. The dose per fraction and its respective beam weightings inputs were provided finally for estimating the MU values. The MU values were calculated as per Equation 2.

The concept of MU ratio was estimated between the TPS calculation MU and hand calculation of MU.

$$MUratio = \frac{TPS calculated MU}{Spreadsheet calculated MU}$$
(3)

Head and neck: The plans usually consisted of bilateral and lower anterior neck (LAN) fields. We have mainly selected tongue cancer and carcinoma of buccal mucosa with the level IV nodal involvements that required lower neck irradiation. Single isocentre was maintained as both the bilateral and LAN fields were of half beam blocked fields to avoid generating hotspots [figure 5].

Treatment plans are normalized by creating a reference point to achieve acceptable planning target volume coverage. Effective area and WED details were obtained from the TPS as described above

Esophagus: The esophagus cases were planned using the traditional approach of delivering adequate dose through oblique fields up to the tolerance of lungs [Figure 6.]

MLCs were used for shielding the organs at risk such as lung. Further additional dose were delivered through AP-PA method. Majority of the treatment plans were normalized on the reference point that gave adequate coverage.

Cervix: Four field box techniques were used for the treatment plans for cervical cancer cases. The plans were normalized either at isocentre or at a reference point (Figure7). MLC leaves were utilized for shielding the organs at risk such as the bladder and rectum.

Results

a) Verification of Open Beam Square Fields(SSD and Isocentric Technique):

The MU required for delivering 200cGy was estimated for mainly three depths of 5cm, 10cm, and 15cm for square fields and fixed SSD of 100cm. The calculated MUs by the spreadsheet and by the TPS are shown in Table 3. The MU ratio values for each field size at all the depths are presented in the table. The mean MU ratios for 5cm, 10cm and 15cm depths were 1.002 ± 0.004 , 1.006 ± 0.007 , & 1.012 ± 0.011 respectively. The comparison of MU for all the above depths is presented in Figure 8.

Similarly, the isocentre-based open beam MUs were estimated by the spreadsheet displayed in Table 4. The mean MU ratio for 5cm,10cm and 15cm depths were 0.999 ± 0.01 , 0.999 ± 0.01 and 1.02 ± 0.01 . MU comparison is exhibited in Figure 9.



| | | Square | Square field size(cm ²) | | | | | | | |
|-------|----------------------------|--------|-------------------------------------|-------|-------|-------|-------|-------|-------|-------|
| Depth | | 4 | 6 | 8 | 10 | 12 | 15 | 20 | 25 | 30 |
| | TPS Calculated MU | 257 | 244 | 237 | 231 | 227 | 221 | 216 | 214 | 209 |
| 5cm | Spread sheet Calculated MU | 257 | 244 | 237 | 231 | 227 | 221 | 216 | 211 | 208 |
| | MU Ratio | 1.002 | 0.999 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.013 | 1.004 |
| | | 4 | 6 | 8 | 10 | 12 | 15 | 20 | 25 | 30 |
| | TPS Calculated MU | 348 | 324 | 310 | 299 | 290 | 281 | 271 | 265 | 259 |
| 10 | Spread sheet Calculated MU | 346 | 325 | 309 | 299 | 290 | 280 | 269 | 260 | 254 |
| 10011 | MU Ratio | 1.005 | 0.998 | 1.004 | 1.002 | 1.000 | 1.003 | 1.009 | 1.019 | 1.018 |
| | | 4 | 6 | 8 | 10 | 12 | 15 | 20 | 25 | 30 |
| | TPS Calculated MU | 473 | 435 | 413 | 393 | 379 | 361 | 346 | 335 | 327 |
| | Spread sheet Calculated MU | 469 | 433 | 409 | 393 | 378 | 358 | 340 | 326 | 317 |
| 15cm | MU Ratio | 1.009 | 1.004 | 1.010 | 1.000 | 1.003 | 1.007 | 1.018 | 1.027 | 1.032 |





TPS: Treatment planning system

Figure 8. Comparison of monitor unit verification calculation at 100cm SSD for 5, 10 and 15 cm depths for isocentric technique

Table 4. Comparison of monitor units between treatment planning system and spreadsheet for isocentric technique

| | | | Square Field Size(Cm ²) | | | | | | | | |
|-------|---------------|----------------------------|-------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Depth | SSD | | 4 | 6 | 8 | 10 | 12 | 15 | 20 | 25 | 30 |
| | | TPS Calculated MU | 234 | 222 | 215 | 210 | 206 | 201 | 197 | 194 | 190 |
| 5 cm | 95 <i>c</i> m | Spread sheet Calculated MU | 234 | 221 | 216 | 211 | 207 | 202 | 198 | 195 | 193 |
| Juli | 95cm | MU Ratio | 1.005 | 0.995 | 0.995 | 0.973 | 0.995 | 0.995 | 0.995 | 0.995 | 0.982 |
| | | | 4 | 6 | 8 | 10 | 12 | 15 | 20 | 25 | 30 |
| | | TPS Calculated MU | 290 | 271 | 258 | 249 | 242 | 234 | 225 | 219 | 215 |
| | | Spread sheet Calculated MU | 290 | 276 | 262 | 252 | 245 | 237 | 227 | 220 | 214 |
| 10cm | 90cm | MU Ratio | 1.00 | 0.982 | 0.986 | 0.989 | 0.987 | 0.989 | 0.992 | 0.994 | 1.004 |
| | | | 4 | 6 | 8 | 10 | 12 | 15 | 20 | 25 | 30 |
| | | TPS Calculated MU | 363 | 331 | 317 | 303 | 291 | 279 | 265 | 256 | 249 |
| 15cm | 85cm | Spread sheet Calculated MU | 363 | 331 | 315 | 301 | 289 | 276 | 264 | 252 | 247 |
| | | MU Ratio | 1.00 | 1.011 | 1.011 | 1.014 | 1.006 | 1.010 | 1.022 | 1.027 | 1.036 |

MU: monitor unit





MUVC for isocentric technique at 5cm, 10,& 15cm depths • 5cm TPS • 5cm SSH • 10cm TPS • 10cm TPS • 10cm TPS • 15cm SSH • 15cm SSH • 15cm SSH

Figure 9. Comparison of monitor unit verification calculation at 100cm SSD for 5, 10, and 15 cm depths for isocentric techniques

Table 5. Comparison of Monitor Units for 15 degree wedge between treatment planning system and spreadsheet for isocentric technique in 5,10,and 15cm depths

| | | | Square Fi | eld Size(cm ² | 2) | | | |
|-------|-------|----------------------------|-----------|--------------------------|--------|--------|--------|--------|
| Depth | SSD | | 4 | 6 | 8 | 10 | 12 | 15 |
| | | TPS calculated MU | 338 | 322 | 310 | 304 | 298 | 292 |
| 5cm | 100cm | Spread sheet Calculated MU | 332.82 | 317.05 | 307.50 | 300.50 | 294.35 | 287.79 |
| | | MU Ratio | 1.016 | 1.016 | 1.008 | 1.012 | 1.012 | 1.015 |
| | | | 4 | 6 | 8 | 10 | 12 | 15 |
| | | TPS Calculated MU | 445 | 423 | 404 | 391 | 380 | 369 |
| 10cm | 90cm | Spread sheet Calculated MU | 449.63 | 421.58 | 400.68 | 387.52 | 376.62 | 363.59 |
| | | MU Ratio | 1.012 | 1.003 | 1.008 | 1.009 | 1.010 | 1.015 |
| | | | 4 | 6 | 8 | 10 | 12 | 15 |
| | | TPS Calculated MU | 618 | 566 | 532 | 512 | 493 | 473 |
| 15cm | 85cm | Spread sheet Calculated MU | 608.61 | 562.40 | 531.02 | 510.09 | 490.40 | 465.21 |
| | | MU Ratio | 1.015 | 1.006 | 1.002 | 1.004 | 1.005 | 1.017 |
| | | | | | | | | |

MU: monitor unit







Table 6. Comparison of Monitor Units for 30-degree wedge between treatment planning system and spreadsheet for isocentric technique in 5, 10 and 15 cm depths

| | | | Square Field Size(cm ²) | | | | | | |
|-------|-------|----------------------------|-------------------------------------|--------|--------|--------|--------|--------|--|
| Depth | SSD | | 4 | 6 | 8 | 10 | 12 | 15 | |
| | | TPS calculated MU | 338 | 322 | 310 | 304 | 298 | 292 | |
| 5cm | 100cm | Spread sheet calculated MU | 332.82 | 317.05 | 307.50 | 300.50 | 294.35 | 287.79 | |
| | | MU ratio | 1.016 | 1.016 | 1.008 | 1.012 | 1.012 | 1.015 | |
| | | | 4 | 6 | 8 | 10 | 12 | 15 | |
| 10cm | 90cm | TPS calculated MU | 445 | 423 | 404 | 391 | 380 | 369 | |
| | | Spread sheet calculated MU | 449.63 | 421.58 | 400.68 | 387.52 | 376.62 | 363.59 | |
| | | MU ratio | 1.012 | 1.003 | 1.008 | 1.009 | 1.010 | 1.015 | |
| | | | 4 | 6 | 8 | 10 | 12 | 15 | |
| 15cm | 85cm | TPS calculated MU | 618 | 566 | 532 | 512 | 493 | 473 | |
| | | Spread sheet calculated MU | 608.61 | 562.40 | 531.02 | 510.09 | 490.40 | 465.21 | |
| | | MU ratio | 1.015 | 1.006 | 1.002 | 1.004 | 1.005 | 1.017 | |

MU: monitor unit

TPS: Treatment planning system

 Table 7. Comparison of Monitor Units for 45-degree wedge between treatment planning system and spreadsheet for isocentric technique and 100 cm SSD

| | | | Square field size(cm ²) | | | | | | |
|-------|-------|----------------------------|-------------------------------------|-------|-------|-------|-------|-------|--|
| Depth | SSD | | 4 | 6 | 8 | 10 | 12 | 15 | |
| | | TPS calculated MU | 529 | 504 | 490 | 475 | 469 | 458 | |
| 5cm | 100cm | Spread sheet calculated MU | 520 | 496 | 485 | 471 | 465 | 455 | |
| | | MU ratio | 1.018 | 1.018 | 1.010 | 1.008 | 1.009 | 1.019 | |
| | | | 4 | 6 | 8 | 10 | 12 | 15 | |
| | 90cm | TPS calculated MU | 702 | 659 | 632 | 611 | 596 | 575 | |
| 10cm | | Spreadsheet calculated MU | 702 | 658 | 626 | 605 | 590 | 571 | |
| | | MU ratio | 1.000 | 1.001 | 1.010 | 1.010 | 1.014 | 1.007 | |
| | | | 4 | 6 | 8 | 10 | 12 | 15 | |
| 15cm | 85cm | TPS calculated MU | 937 | 869 | 826 | 789 | 765 | 733 | |
| | | Spreadsheet calculated MU | 950 | 875 | 829 | 796 | 765 | 730 | |
| | | MU ratio | 0.986 | 0.993 | 0.996 | 0.991 | 0.999 | 1.009 | |

MU: monitor unit

TPS: Treatment planning system

MUVC verification for 45 degree wedge at 5cm,10cm & 15cm depth for



Figure 12. Comparison of monitor unit verification calculation for 5, 10 and 15 cm depths for 45 degree wedge for 100 cm SSD

b) Verification of Physical Wedged Fields(Isocentric Technique):

Tables 5, 6, and 7 demonstrate the MU estimated from spreadsheet for 15°, 30° and 45° wedges and the MU estimated for the same setup by the TPS. The comparison of MU between TPS and spreadsheet is shown in figures 10, 11, and 12 for wedge angles 15, 30 and 45. The wedge factors were applied while calculating MU for the respective wedges. The average MU ratios for 15 degree wedges in 5cm, 10cm and 15cm depths were 0.992 \pm 0.009, 0.991 \pm 0.006, and 1.015 \pm 0.011, respectively.

For estimating MU for 30 degree wedge angle, wedge factors were applied in the spreadsheet. The

calculated MU by spreadsheet increased as the wedge angle increased from 15 degree to 30 degree. The average MU ratios for 30 degree wedge angle in 5cm,10cm, and 15cm depths were 1.013 ± 0.003 , 1.009 ± 0.004 and 1.008 ± 0.006 , respectively.

A similar approach was adopted for estimating MU for 45 degree wedge angle; MU ratio was estimated for 5cm, 10cm, and 15cm depths; the average MU ratios were 1.0317 ± 0.005 , 1.007 ± 0.005 , and 0.995 ± 0.007 , respectively.



c) Verification of 3DCRT Treatment Plans(Isocentre- Based Plans):

MUs for conformal radiotherapy plans were verified between TPS and spreadsheet for head and neck, esophageal and cervical cancers. Forty fields were taken for the evaluation of each case. All the fields were of open fields shaped by MLC. The comparison parameters were tabulated in tables 8, 9, and 10 for head and neck, esophageal and cervical cancers respectively. The comparison diagram for both methods of MU calculation is depicted in figures 13, 14, and 15.

Mean MU ratio and average percentage deviation were calculated using the TPS and spreadsheet MU values. The average MU ratios for open fields for head and neck, cervical and esophageal cancers were 0.995 ± 0.024 , 1.012 ± 0.029 , and 1.026 ± 0.040 respectively. The observed average percent deviation for the above mentioned sites between TPS and spreadsheet calculations were 0.048, 1.16, and 2.45, respectively.

Table 8. Comparison of Monitor Units for head and neck cancers between treatment planning systems and spreadsheet

| | Field | | | | | | | |
|-------|-------|-----------|-----------|------------------------|--------|---------|----------|-------------|
| Field | name | Dose(cGy) | Depth(cm) | Area(cm ²) | MU TPS | MU calc | MU ratio | % Deviation |
| 1 | Bilat | 100 | 4.9 | 101.61 | 101 | 102 | 0.99 | -0.99 |
| 2 | Bilat | 100 | 5.3 | 105.21 | 105 | 107 | 0.981 | -1.905 |
| 3 | LAN | 200 | 3.3 | 108.23 | 204 | 202.3 | 1.008 | 0.833 |
| 4 | Bilat | 92.8 | 5.9 | 139.45 | 98 | 97 | 1.01 | 1.02 |
| 5 | Bilat | 7.2 | 5.9 | 107.13 | 8 | 8 | 1 | 0 |
| 6 | Bilat | 92.8 | 5 | 144.7 | 98 | 98.1 | 0.999 | -0.102 |
| 7 | LAN | 7.2 | 5 | 102.77 | 8 | 8 | 1 | 0 |
| 8 | Bilat | 90.4 | 8 | 118.08 | 104 | 105 | 0.99 | -0.962 |
| 9 | LAN | 153.8 | 2.4 | 103.7 | 155 | 154 | 1.006 | 0.645 |
| 10 | LAN | 46.2 | 14.5 | 103.7 | 55 | 57 | 0.965 | -3.636 |
| 11 | Bilat | 100 | 5.5 | 112.79 | 103 | 106 | 0.972 | -2.913 |
| 12 | Bilat | 100 | 4.9 | 117.04 | 101 | 102 | 0.99 | -0.99 |
| 13 | LAN | 200 | 1 | 88.9 | 197 | 208 | 0.947 | -5.584 |
| 14 | Bilat | 100 | 5.3 | 124.65 | 103 | 105 | 0.981 | -1.942 |
| 15 | Bilat | 100 | 5.7 | 123.17 | 103 | 105 | 0.981 | -1.942 |
| 16 | LAN | 200 | 2.3 | 84.63 | 196 | 200 | 0.98 | -2.041 |
| 17 | Bilat | 95.6 | 6.8 | 136.88 | 101 | 102 | 0.99 | -0.99 |
| 18 | Bilat | 5.4 | 6.8 | 80.19 | 6 | 6 | 1 | 0 |
| 19 | Bilat | 94.2 | 6.6 | 136.88 | 102 | 101.3 | 1.007 | 0.686 |
| 20 | Bilat | 4.8 | 6.6 | 78.65 | 5 | 5 | 1 | 0 |
| 21 | LAN | 200 | 1 | 124.88 | 200 | 204 | 0.98 | -2 |
| 21 | Bilat | 100 | 5 | 102.53 | 106 | 107.78 | 0.983 | -1.679 |
| 22 | Bilat | 100 | 4.5 | 103.21 | 104 | 103.56 | 1.004 | 0.423 |
| 23 | LAN | 200 | 3.5 | 109.21 | 202 | 201.48 | 1.003 | 0.257 |
| 24 | Bilat | 92.5 | 5.5 | 137 | 97 | 97.08 | 0.999 | -0.082 |
| 25 | Bilat | 8.5 | 6.5 | 111 | 7 | 7.1 | 0.986 | -1.429 |
| 26 | Bilat | 94 | 4.5 | 148 | 96 | 95.5 | 1.005 | 0.521 |
| 27 | LAN | 8 | 4.5 | 148 | 8 | 8.12 | 0.985 | -1.5 |
| 28 | Bilat | 95 | 7.5 | 120 | 103 | 104.96 | 0.981 | -1.903 |
| 29 | LAN | 158 | 2.5 | 106 | 153 | 155.86 | 0.982 | -1.869 |
| 30 | LAN | 45 | 4.5 | 105 | 45 | 46.58 | 0.966 | -3.511 |
| 31 | Bilat | 100 | 5 | 114 | 108 | 107.17 | 1.008 | 0.769 |
| 32 | Bilat | 100 | 4.5 | 118 | 104 | 102.87 | 1.011 | 1.087 |
| 33 | LAN | 200 | 2.5 | 92 | 197 | 198.8 | 0.991 | -0.914 |
| 34 | Bilat | 100 | 5 | 124 | 105 | 106.64 | 0.985 | -1.562 |
| 35 | Bilat | 100 | 5.7 | 122.17 | 106 | 105.29 | 1.007 | 0.67 |
| 36 | LAN | 200 | 2.5 | 84.63 | 200 | 199.15 | 1.004 | 0.425 |
| 37 | Bilat | 95.6 | 6.8 | 136.88 | 104 | 102.53 | 1.014 | 1.413 |
| 38 | Bilat | 6.5 | 6.7 | 82.12 | 8 | 7.2 | 1.111 | 10 |
| 39 | Bilat | 96 | 6 | 135.21 | 103 | 104.69 | 0.984 | -1.641 |
| 40 | Bilat | 5.2 | 6.5 | 81.21 | 6 | 5.79 | 1.036 | 3.5 |



1



Figure 13a

Figure 13b

Figure 13. Comparison of monitor unit (MU) for head and neck treatment: 13a: MU comparison between treatment planning system(TPS)and spreadsheet calculations;13b) MU ratio calculated between TPS and spreadsheet

| | Table 9 |). C | lompari | son of | f monito | r units f | or cervica | l cancer | between | treatment | planning | system and | l spreadsh | eet |
|--|---------|-------------|---------|--------|----------|-----------|------------|----------|---------|-----------|----------|------------|------------|-----|
|--|---------|-------------|---------|--------|----------|-----------|------------|----------|---------|-----------|----------|------------|------------|-----|

| | Field | | | | | | | |
|-------|--------|-----------|-----------|------------------------|--------|---------|----------|-------------|
| Field | name | Dose(cGy) | Depth(cm) | Area(cm ²) | MU TPS | MU calc | MU ratio | % Deviation |
| 1 | Lt Lat | 49.4 | 16.1 | 216.6 | 73 | 70.79 | 1.031 | 3.015 |
| 2 | AP | 42 | 11.4 | 299.51 | 51 | 49.51 | 1.03 | 2.91 |
| 3 | Rt Lat | 49.4 | 16.4 | 217.04 | 73 | 70.29 | 1.038 | 3.701 |
| 4 | PA | 59.2 | 8.5 | 285.59 | 65 | 64.59 | 1.006 | 0.625 |
| 5 | AP | 55 | 8.2 | 234.08 | 61 | 61.02 | 1 | -0.039 |
| 6 | Lt Lat | 50 | 14.3 | 166.38 | 71 | 68.29 | 1.04 | 3.815 |
| 7 | PA | 45 | 9 | 241.78 | 50 | 51.52 | 0.97 | -3.045 |
| 8 | Rt Lat | 50 | 14.2 | 168.04 | 69 | 68.42 | 1.008 | 0.84 |
| 9 | Lt Lat | 51.2 | 17.2 | 201.55 | 78 | 76.02 | 1.026 | 2.534 |
| 10 | AP | 30.8 | 10.8 | 299.34 | 37 | 35.19 | 1.051 | 4.865 |
| 11 | Rt Lat | 51.2 | 14.9 | 192.55 | 73 | 68.24 | 1.07 | 6.518 |
| 12 | PA | 66.6 | 10.4 | 264.61 | 79 | 77.27 | 1.022 | 2.178 |
| 13 | AP | 47.6 | 9.4 | 313.87 | 54 | 53.16 | 1.016 | 1.554 |
| 14 | PA | 57.2 | 9 | 291.49 | 65 | 64.72 | 1.004 | 0.43 |
| 15 | Lt Lat | 47.6 | 18 | 214.84 | 70 | 72.43 | 0.966 | -3.476 |
| 16 | Rt Lat | 47.6 | 17.3 | 211.58 | 70 | 69.90 | 1.001 | 0.129 |
| 17 | AP | 40 | 11.8 | 288.28 | 49 | 46.98 | 1.043 | 4.117 |
| 18 | PA | 60 | 9.1 | 257.99 | 69 | 68.26 | 1.011 | 1.059 |
| 19 | Lt Lat | 50 | 17.1 | 199.29 | 78 | 74.44 | 1.048 | 4.556 |
| 20 | Rt Lat | 50 | 17.3 | 199.88 | 78 | 74.08 | 1.053 | 5.017 |
| 21 | Lt Lat | 46.8 | 18 | 190.62 | 75 | 72.56 | 1.034 | 3.246 |
| 22 | Lt Lat | 3.6 | 18 | 70.43 | 6 | 6.21 | 0.965 | -3.586 |
| 23 | AP | 36.4 | 9.7 | 252.11 | 43 | 41.00 | 1.049 | 4.65 |
| 24 | Rt Lat | 46.8 | 16.4 | 187.16 | 72 | 67.75 | 1.063 | 5.893 |
| 25 | Rt Lat | 3.6 | 16.4 | 72.48 | 6 | 5.70 | 1.053 | 4.993 |
| 26 | PA | 62.6 | 10.2 | 242.88 | 75 | 73.55 | 1.02 | 1.928 |
| 27 | Lt Lat | 52.1 | 15 | 217 | 71 | 72.04 | 0.986 | -1.465 |
| 28 | AP | 49 | 10.5 | 294 | 55 | 56.4 | 0.975 | -2.545 |
| 29 | Rt Lat | 48 | 15.5 | 215 | 67 | 66.02 | 1.015 | 1.463 |
| 30 | PA | 58 | 9 | 287 | 68 | 65.79 | 1.034 | 3.25 |
| 31 | AP | 53 | 7.5 | 231 | 55 | 56.95 | 0.966 | -3.545 |
| 32 | Lt Lat | 48 | 14 | 168.21 | 64 | 65.98 | 0.97 | -3.094 |
| 33 | PA | 47 | 8 | 238.23 | 51 | 52.34 | 0.974 | -2.627 |
| 34 | Rt Lat | 48.5 | 15.2 | 165.21 | 68 | 69.02 | 0.985 | -1.5 |
| 35 | Lt Lat | 52.21 | 16.5 | 210.21 | 74 | 74.19 | 0.997 | -0.257 |
| 36 | AP | 31.5 | 10 | 311.12 | 36 | 36.51 | 0.986 | -1.417 |
| 37 | Rt Lat | 49.45 | 16 | 195 21 | 72 | 71 71 | 1 004 | 0.403 |
| 38 | PA | 63.21 | 10 21 | 267.21 | 75 | 73.63 | 1.001 | 1 827 |
| 39 | AP | 49 21 | 85 | 316.21 | 52 | 53 38 | 0.974 | -2 654 |
| 40 | DA | 55 2 | 0.5 | 205 21 | 62 | 61 76 | 1 004 | 0.287 |
| 10 | 1 11 | JJ.4 | 7.1 | 473.41 | 04 | 01./0 | 1.007 | 0.00/ |

MU: monitor unit





Figure14.Comparison of monitor unit (MU) for cervical treatment plans; 14a) MU comparison between TPS and spreadsheet. 14b) MU ratio calculated between TPS and spreadsheet

| Field | Field name | Dose(cGy) | Depth(cm) | Area(cm ²) | MU TPS | MU calc | MU ratio |
|-------|------------|-----------|-----------|------------------------|--------|---------|----------|
| 1 | Oblique | 83.8 | 9.6 | 94 | 95.54 | 0.984 | -1.64 |
| 2 | PA | 9.4 | 9.6 | 12 | 11.62 | 1.032 | 3.119 |
| 3 | Oblique | 93 | 8.5 | 104 | 103.31 | 1.007 | 0.66 |
| 4 | Oblique | 14 | 8.5 | 17 | 16.95 | 1.003 | 0.256 |
| 5 | AP | 100 | 9.3 | 112 | 113.67 | 0.985 | -1.5 |
| 6 | PA | 100 | 9.5 | 118 | 114.53 | 1.03 | 2.941 |
| 7 | AP | 5 | 7.9 | 48 | 44.8 | 1.071 | 6.667 |
| 8 | AP | 89.6 | 7.9 | 8 | 7.9 | 1.013 | 1.25 |
| 9 | Oblique | 6 | 11.1 | 9 | 8 | 1.125 | 11.111 |
| 10 | Oblique | 99.6 | 11.1 | 128 | 128.57 | 0.996 | -0.447 |
| 11 | PA | 94.4 | 9.3 | 111 | 115.09 | 0.964 | -3.692 |
| 12 | AP | 94.4 | 6.3 | 107 | 104.31 | 1.026 | 2.509 |
| 13 | AP | 5.6 | 9.3 | 7 | 7.21 | 0.97 | -3.123 |
| 14 | AP | 5.6 | 6.3 | 7 | 6.48 | 1.079 | 7.338 |
| 15 | Oblique | 57.2 | 12.9 | 76 | 75.86 | 1.002 | 0.174 |
| 16 | PA | 57.2 | 10.8 | 72 | 71.02 | 1.014 | 1.347 |
| 17 | AP | 57.2 | 10.9 | 69 | 70.98 | 0.972 | -2.871 |
| 18 | Oblique | 28.6 | 10 | 38 | 36.14 | 1.051 | 4.886 |
| 19 | AP | 85.8 | 6.8 | 97 | 94.67 | 1.025 | 2.393 |
| 20 | AP | 85.8 | 5.5 | 41 | 40 | 1.025 | 2.439 |
| 21 | PA | 14.2 | 6.8 | 7 | 7.1 | 0.986 | -1.429 |
| 22 | AP | 14.2 | 5.5 | 6 | 5.5 | 1.091 | 8.333 |
| 23 | PA | 97.4 | 8.7 | 108 | 109.59 | 0.985 | -1.478 |
| 24 | PA | 7 | 8.7 | 8 | 8.20 | 0.975 | -2.61 |
| 25 | PA | 88.4 | 9.4 | 105 | 102.95 | 1.02 | 1.947 |
| 26 | PA | 7 | 9.4 | 10 | 8.78 | 1.138 | 12.144 |
| 27 | AP | 87.2 | 10.6 | 107 | 104.56 | 1.023 | 2.278 |
| 28 | AP | 97.8 | 9 | 118 | 114.78 | 1.028 | 2.722 |
| 29 | AP | 5.8 | 10.6 | 8 | 7.46 | 1.071 | 6.63 |
| 30 | PA | 9.4 | 9 | 12 | 11.89 | 1.009 | 0.914 |
| 31 | PA | 66.6 | 6.8 | 77 | 74.40 | 1.035 | 3.366 |
| 32 | AP | 63.4 | 8.8 | 77 | 75.38 | 1.021 | 2.097 |
| 33 | AP | 26.6 | 5.2 | 31 | 29.37 | 1.055 | 5.256 |
| 34 | AP | 43.4 | 7.1 | 56 | 51.32 | 1.091 | 8.347 |
| 35 | AP | 93 | 6.8 | 106 | 101.00 | 1.049 | 4.712 |
| 36 | PA | 74.4 | 8.8 | 88 | 86.21 | 1.021 | 2.033 |
| 37 | AP | 9.4 | 6.8 | 11 | 10.92 | 1.007 | 0.718 |
| 38 | PA | 9.4 | 8.8 | 12 | 11.55 | 1.039 | 3.71 |
| 39 | AP | 120 | 5.4 | 125 | 122.08 | 1.024 | 2.332 |
| 40 | PA | 80 | 10.8 | 94 | 91.90 | 1.023 | 2.226 |

MU: monitor unit





Figure 15. Comparison of monitor unit (MU) for esophageal cancer treatment plans; 15a) MU comparison between treatment planning system (TPS) and spreadsheet. 15b) MU ratio calculated between treatment planning system (TPS) and spreadsheet

d) Summary of MU Comparison Between TPS And Spreadsheet

The summary of MU ratio and percentage of deviation for SSD and isocentric methods are shown in table 11a. Similarly, the MU ratio details for physical wedges are presented in table 11b.

The statistical significance between the TPS calculated MU and spreadsheet calculated MU was estimated through paired t -test and tabulated is tabulatedin11c. No significant difference was observed between the two methods of calculation.

Table 11a. Mean monitor unit ratio and percentage deviation for square fields for fixed SSD and isocentric method

| | Mean MU ratio | | | Percentage deviation from TPS | | | |
|--|-------------------|------------------|-----------------|-------------------------------|----------------|--------------|--|
| Square fields @ 100cm SSD | 5cm | 10cm | 15cm | 5cm | 10cm | 15cm | |
| | 1.002 ± 0.004 | 1.006±0.007 | 1.012 ± 0.011 | 0.208±0.474 | 1.205±1.06 | 0.611±0.800 | |
| Isocentric Square fields | 0.999 ± 0.01 | 0.999 ± 0.01 | 1.02 ± 0.01 | 452±0.536 | -0.889 ± 0.753 | 0.644 ±0.494 | |
| MIL monitor unit TDC. Treatment planning quatern | | | | | | | |

MU: monitor unit TPS: Treatment planning system

Table 11b. Mean monitor unit ratio and percentage deviation for physical wedges

| | Wedge | Mean MU ratio | | | Percentage deviation from TPS | | | |
|-------|-----------|--------------------|-------------------|-------------------|-------------------------------|-------------------|----------------|--|
| | angle | 5cm | 10cm | 15cm | 5cm | 10cm | 15cm | |
| | 15 degree | 0.992 ± 0.009 | 0.991±0.006 | 1.015 ± 0.011 | -0.452 ± 0.536 | 0.889 ± 0.753 | -0.644 ± 0.494 | |
| | 30 degree | 1.013 ± 0.003 | 1.009 ± 0.004 | 1.008 ± 0.006 | 1.109 ± 0.431 | 0.630 ± 0.446 | -0.486 ± 0.643 | |
| _ | 45 degree | 1.0317 ± 0.005 | 1.007 ± 0.005 | 0.995 ± 0.007 | 1.104 ± 0.421 | 0.741 ± 0.321 | 0.846±0.123 | |
| 3 6 1 | r •. •. | | 1 | | | | | |

MU: monitor unit TPS: Treatment planning system

Table 11c. Mean monitor unit ratio and percentage of deviation for head and neck, cervical and esophageal cases

| | Number of fields | Mean MU ratio | Percentage deviation from TPS | Statistical significance |
|---------------|------------------|-------------------|----------------------------------|--------------------------|
| Head and neck | 40 | 0.995 ± 0.024 | -0.483 ± 2.33 | 0.013 |
| Cervix | 40 | 1.012 ± 0.029 | 1.166 ± 2.915 | 0.006 |
| Esophagus | 40 | 1.026 ± 0.040 | 2.451 ± 3.70 | 0.001 |
| | | | | |

MU: monitor unit TPS: Treatment planning system

Discussion

In this work, we sought to estimate the accuracy of in-house developed spreadsheet with TPS. The comparison was made for fixed SSD beams, Isocentric open square fields, and isocentric based 3D conformal treatment plans for head and neck, cervical cancers.

As per TG-40, the acceptable deviation for the secondary MU check is 2%. The average percentages of deviation for open square fields were 0.208, 1.205, and 0.611. Smaller deviations were expected due to the uniformity of square fields and the homogenous

phantom medium taken for dose calculation. The MU values for isocentric beams gave the percentage of deviations of -0.452, -0.889, and 0.644 from the TPS values. In our designed spreadsheet, the TMR values were calculated from the measured PDD values; a similar method of calculation was incorporated in most of the commercial TPSs. The lesser deviation ensured that the spreadsheet can be used for both methods of, SSD and SAD-based treatment. Additionally it ensured that the traditional method of estimating the TMR values from the measured PDD values can still be continued.

The mean MU ratios for square fields for fixed SSD technique and isocentre beams were within the acceptable range for the taken depths of 5cm, 10cm, and 15cm. We observed a higher value of 1.02 ± 0.01 for 15cm depth. The overall MU ratio lies within the range of 0.999 to 1.02 for square field geometries, which shows a deviation of 1% between the TPS calculation and the spread sheet calculation. Chanetal [7] and Starkshallet al[10].presented similar results in their studies. These two authors showed their work on the Pinnacle planning system and they presumed that the deviation may be due to precision in determining the beam entry point while other factors are kept constant.

The percentage of deviation of MU for the three physical wedges of 15, 30, and 45 degree were estimated for three depths, namely 5cm, 10cm, and 15cm listed in table 11b. It is observed that the entire physical wedge MUs estimated by the spreadsheet were within the acceptable tolerance of 2%. Higher deviations of 1.109 and 1.104were observed for 30 and 45 degree wedges at 5cm depth; this deviation was also under the recommended tolerance of 2%.

The 15 degree wedges had the mean MU ratio of 0.992 for 5cm and 10cm depths and 1.015 for 15 cm depth. This ensured that the open beam geometries with wedge as the only beam modifying device had a good agreement with the TPS dose calculations. It was anticipated that the MU ratio should be near unity for these simple geometric fields in the absence of in heterogeneities, filed shape irregularities, and off axis corrections.

The MU ratios were estimated for head and neck, cervix and esophagus cases only. A total of 40 fields for each treatment site were taken for estimation. The MU ratio was 0.995 for Head and Neck plans and 1.012 for cervix plans with standard deviations of 0.024 and 0.029 respectively. However we observed that mean MU ratio for esophagus plans was 1.026 with the standard deviation of 0.040. This higher deviation from the TPS should be addressed. This deviation may be due to the heterogeneity, and lung tissue interface present in the beam path. This type of deviations can be well accounted by highly overcome sophisticated algorithms. То the deviations in the heterogeneity situations, the spreadsheet should be configured for accounting the situations. The limitation of the present spreadsheet was of lack of accounting for the difference in tissue densities. Konrad et al [11] also observed that the independent MU checks have limitations in heterogeneity situations and mentioned that the accuracy varies with treatment site.

The development of spreadsheets for MUVC is addressed by several authors. Independent MU checks are essential to ensure delivering the proper dose to the patients to achieve the ICRU recommendations. This study was performed for a limited number of fields for mostly treated sites in our institution. MUVC verifications gave the accuracy levels of our TPS system for the tested cases. The framing of spreadsheet needs inputs such as PDD, O.F and O.A.R. In our study we obtained the TMR values used for isocentric calculations from the traditional approach of obtaining TMR from PDD values. The resulted MU values also provided evidence that the PDD values can be used for estimating TMR values without the need for separate TMR measurement. Our spreadsheet design and approach is also similar method of TPS estimating TMR from the measured PDD values.

The necessity and advantages of the independent MU check system is recognized through this study. Our study indicated that the spreadsheet MU calculation can be corroborated to the TPS planning when the plans are normalized at the isocentre, or any reference point.

The limitations of the spreadsheet were also considered .The advancements in treatment techniques may comprise non-coplanar beams, and modulated fields increase the complexity in spreadsheet design. Our spreadsheet still needs to be improved to accommodate the various complex treatment techniques. Presently, the inputs for the spreadsheets were manually entered. There is need for designing a spreadsheet that has the capability to accept data through electronic transfer, so that the same spreadsheet configuration can be extended for various machines and beam qualities.

Conclusion

The independent spreadsheet was designed and tested for most of the routine treatment sites and geometries. The designed spreadsheet had good agreement with the Eclipse TPS, version 13.8, for homogenous treatment sites such as head and neck and cervix. The accuracy reduces in case of heterogeneous tissues such as the esophagus; however, the accuracy is still within tolerance. The inclusion of parameters to account for tissue homogeneity in the spreadsheet has to be considered.

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